

## Eclipse Observations of Coronal Emission Lines. I. [Fe x] 6374Å Profiles at the Eclipse of 16 February 1980

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**Abstract.** Coronal spectra during the total solar eclipse of 1980 February 16, were obtained in the 6374Å [Fe x] line using a multislit spectrograph. These spectra have a dispersion of  $2.5 \text{ \AA mm}^{-1}$ . The observed line profiles from  $1.1$  to  $1.7 R_{\odot}$  with a spatial resolution of  $10 \times 22 \text{ arcsec}^2$ , give half-widths that vary between  $0.6 \text{ \AA}$  and  $2.4 \text{ \AA}$ . A large number of locations have half-widths around  $1.3 \text{ \AA}$  corresponding to a temperature of  $4.6 \times 10^6 \text{ K}$ . If temperature of the order of  $1.3 \times 10^6 \text{ K}$  are typical of the regions that emit [Fe x], then turbulent velocities of  $\sim 30 \text{ km s}^{-1}$  need to be invoked for the enhanced line broadening. The line-of-sight velocities measured range between  $+14 \text{ km s}^{-1}$  to  $-17 \text{ km s}^{-1}$ . Most of the locations have velocities less than  $\pm 5 \text{ km s}^{-1}$ . From these observations we conclude that corona does not show any localized differential mass motion and that it co-rotates with the photospheric layers deeper down.

**Key words:** Solar corona — red coronal line — turbulent velocities — rotation of solar corona

### 1. Introduction

Much information on the physical characteristics of the solar corona can be evaluated from the study of emission-line profiles of the forbidden lines in the coronal spectrum at a total solar eclipse. They permit us to determine the spatial dependence of kinetic temperature or the influence of turbulent velocities that contribute to the enhanced broadening of the line profile. Such studies help us attain an improved understanding of the coronal heating mechanism and the gradients of temperature that contribute to solar wind outflow. The advantage of the total eclipse lies in providing a minimum of scattered-light background and Fraunhofer-line contamination, factors that normally restrict the coronagraph in providing similar information with the aid of an artificial eclipse.

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Line-profile measures for temperature evaluation have in the recent past been used mostly with coronagraphs. At eclipses, such measures have almost exclusively been carried out with Fabry-Perot interferometers both in the two-dimensional mode by photographic techniques and at a few specific locations by photoelectric scan methods. Such slitless evaluations pioneered by Jarrett and von Klüber (1955, 1961) have been used at subsequent eclipses by Delone and Makarova (1969), Marshall and Henderson (1973), Liebenberg, Bessey and Watson (1975) and Chandrasekhar, Desai and Angreji (1981). The Fabry-Perot instrumentation has the advantage of simultaneous registration of interference fringes over most of the corona, from which a line profile can be evaluated; the disadvantage is the uncertainty of the contribution by Doppler-shifted elements to the line profile and which is inherent in a slitless mode. Such limitations are absent in a slit survey, since the finite width of the slit samples a limited areal extent of the corona. On the other hand, the slit permits the acquisition of information only along the coronal emission regions intercepted by its length, and hence the multiplicity of spatial information collected by the Fabry-Perot technique is missing. Procedures to minimize this handicap, however, do exist and have been used for other purposes at recent solar eclipses (Livingston, Harvey and Doe 1970). The multislit technique has been used by the Kitt Peak investigators only for measures of coronal rotation. It is, however, a technique that can be used to provide a good two-dimensional coverage of the corona by judicious choice of instrumentation and spatial sequencing at the eclipse and has all the advantages to offer which standard slit spectroscopy does over its slitless counterpart.

## 2. Instruments

An objective of 14 cm aperture and 140 cm focal length formed an image of the sun on the multislit spectrograph. The doublet was corrected for the 6500 Å region and was fed by a single mirror 45-cm coelostat with Zerodur optics, and a well-regulated stepper-motor friction drive. The multislit spectrograph functioned in the Littrow mode with a 600-line grating that gave a dispersion of  $2.5 \text{ \AA mm}^{-1}$  in the fourth order red. Four entrance slits, each separated by 5 mm from its neighbour, together formed the multislit. The slits, therefore, were spaced 12.3 arcmin on the solar image. An interference filter of 9.5 Å pass-band and peaked at 6374 Å was used in front of the multislit. In the Littrow focal plane, four spectra originating from the multislit each about 10 Å in width—were stacked side by side on the photocathode of a single-stage Varo image intensifier. The image intensifier has a gain of 20 and an effective aperture of 30 mm. A plate-holder magazine enabled rapid change-over of the emulsion that had to be in contact with the fibre-optic faceplate. Each spectrum has a neon comparison. Since these spectral lines were not filtered by the interference filter, there were many lines from overlapping orders available that permitted velocity measurements by comparison.

## 3. Observations

Two of the three plates exposed during the total phase of the eclipse have been used in this study. The third had to be discarded because of excessive tube back-

ground that had accumulated by virtue of the hot afternoon and the fact that the image tube had been turned on in readiness for the event several minutes before totality. The exposures used were both of 45 s duration and enabled emission lines to be detected to distances as far as  $1.7 R_{\odot}$ . Between the first and second exposures, the solar image was shifted through 4.5 arcmin along the axis of rotation in order to sample a new set of coronal regions with the multislit. The orientation of the multislit was along position angle  $89.5^{\circ}$ . The spectra were exposed on Eastman 103a-D emulsion and developed in D-19 at  $20^{\circ}\text{C}$  for five minutes together with the step-wedge calibration obtained immediately after the eclipse with the same spectrograph. Neon spectra obtained along the entire length of the four slits permitted the evaluation of the instrumental line profiles at several points of each slit. We show in Fig. 1 the values of full width at half maximum (FWHM) of these instrumental line profiles at several points on each slit and the final mean value assigned to each for determination of coronal line widths.

Microphotometer scans of these spectra have been obtained with a projected slit size of  $4.5 \times 22 \text{ arcsec}^2$  on the plate. Successive scans have been made that were separated by 30 arcsec along the slit. This spacing had to be increased to 45 or 50 arcsec at locations where the ratio of maximum line intensity to continuum intensity was low. The transmission curve of the narrow interference filter was evaluated with the aid of the solar spectrum and the Kodaikanal 18-m spectrograph. Working at a

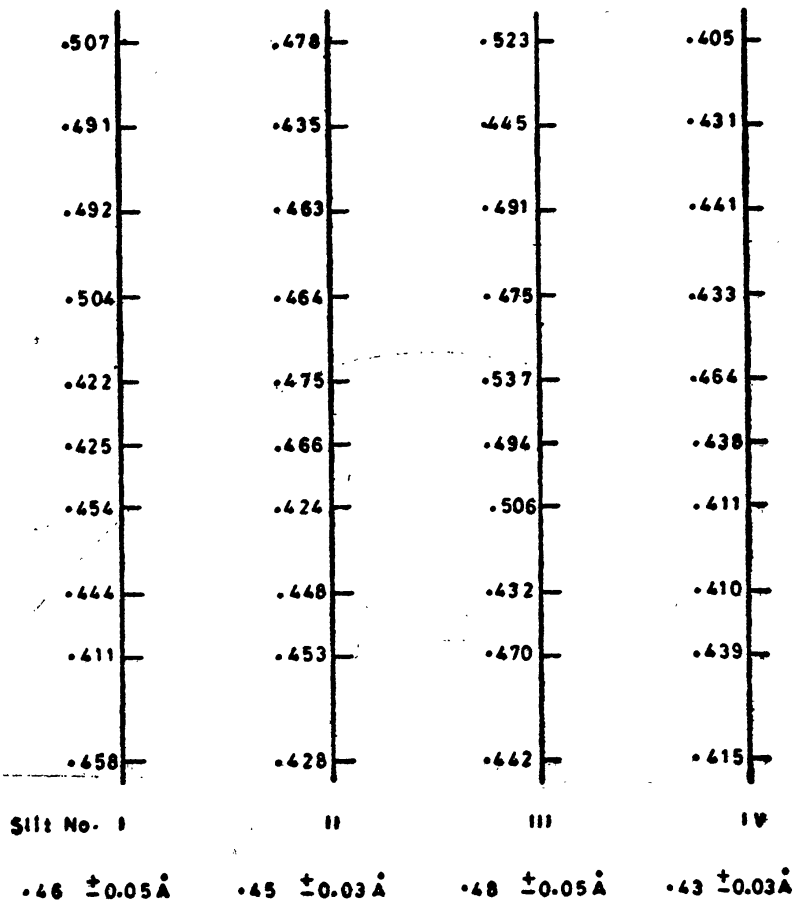


Figure 1. Full width at half maximum of instrumental line profile at various locations on the slits. Mean value is indicated below each slit.

dispersion of  $9 \text{ mm } \text{\AA}^{-1}$ , transmission spectra through several different regions of the interference filter—each spaced 5 mm from its neighbour, have been used in the evaluation of the average filter characteristic. The normalized mean transmission curve of the filter thus obtained is used to operate on the intensity curve of the red coronal line, as evaluated at each point along the slit (Fig. 2). The procedure gives the observed profile of the coronal line. The FWHM is corrected for instrumental line-width using the data of Fig. 1 and the assumption that both profiles are gaussian.

Image-tube spectra usually call for extra precautions in radial-velocity measurements over those photographed directly, due to the pin-cushion effect of the image intensifier. We have used the full-length neon spectra and made dispersion measures at several points along the length in terms of a fiducial reference of a cross hair placed against the slits during the eclipse and the measures that followed immediately after. The  $6374 \text{ \AA}$  line was flanked on either side by the neon lines  $8495.36 \text{ \AA}$  (third order spectrum) and  $6382.99 \text{ \AA}$  of the normal fourth order. The Doppler displacements of the line as a whole were evaluated from microphotometer scans that included the neon comparison lines as well. The velocity measures were spaced 30 arcsec along each slit.

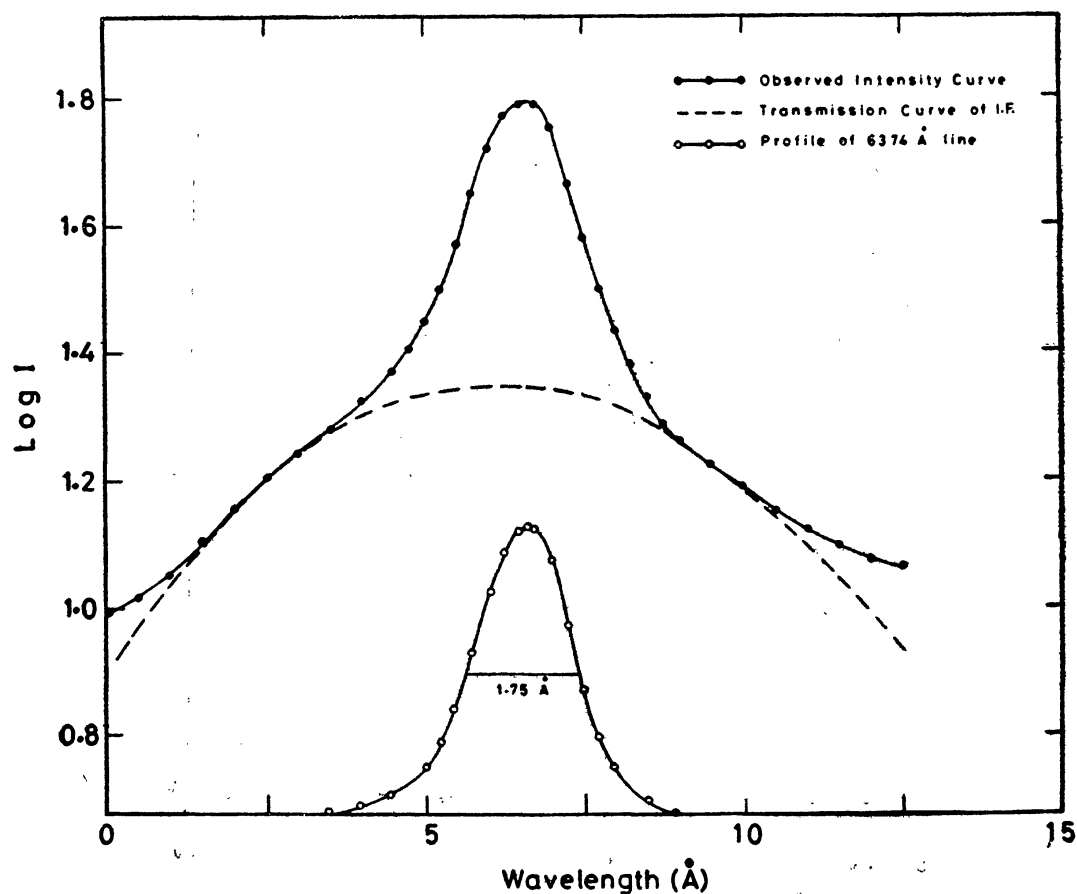


Figure 2. A typical line profile of  $[\text{Fe x}] 6374 \text{ \AA}$  at one of the locations of corona is shown. Full line is a plot between  $\log I$  and wavelength whereas the dotted one is the transmission curve of the interference filter on the same scale. Shown below is the line profile plotted as intensity versus wavelength, after correction for the transmission of the interference filter.

## 4. Results

We have measured the widths of the red coronal line at 236 locations in the solar corona. These locations range from  $1.1 R_{\odot}$  to  $1.7 R_{\odot}$  and aim to give a satisfactory coverage all around the solar limb. The data are presented in Table 1. The position angle measured from the north point of the projected axis of solar rotation and the radial distance from the centre of the disc are given in Columns (2) and (3). The values of FWHM are in Column (4) while those in Column (5) express turbulent velocities derived by assuming the temperature of corona to be  $1.3 \times 10^6$  K. In Columns (6) and (7) we give the peak brightness of the continuum at the line centre as well as the peak brightness of the line. This is expressed as a ratio in Column (8) and serves to portray the localized enhancements of the line emission to that of the background K corona.

Table 1. Line widths, intensities and turbulent velocities derived from the red coronal line.

| No.         | Position angle $\theta$ | $R/R_{\odot}$ | FWHM $\text{\AA}$ | $V_t$ $\text{km s}^{-1}$ | $I_c$ | $I_{\max}$ | $\frac{I_{\max}}{I_c}$ |
|-------------|-------------------------|---------------|-------------------|--------------------------|-------|------------|------------------------|
| (1)         | (2)                     | (3)           | (4)               | (5)                      | (6)   | (7)        | (8)                    |
| Slit IV (1) |                         |               |                   |                          |       |            |                        |
| 1           | 322.9                   | 1.437         | 1.34              | 29                       | 19    | 34         | 1.79                   |
| 2           | 323.4                   | 1.428         | 1.40              | 32                       | 18    | 32         | 1.78                   |
| 3           | 323.9                   | 1.418         | 1.11              | 19                       | 22    | 42         | 1.91                   |
| 4           | 324.4                   | 1.409         | 1.12              | 20                       | 19    | 41         | 2.16                   |
| 5           | 324.9                   | 1.400         | 1.23              | 25                       | 25    | 47         | 1.88                   |
| 6           | 325.4                   | 1.391         | 1.29              | 28                       | 23    | 46         | 2.00                   |
| 7           | 325.9                   | 1.382         | 1.30              | 28                       | 29    | 53         | 1.83                   |
| 8           | 327.0                   | 1.365         | 1.33              | 29                       | 31    | 47         | 1.52                   |
| 9           | 328.1                   | 1.349         | 1.23              | 25                       | 47    | 66         | 1.40                   |
| 10          | 329.2                   | 1.332         | 1.41              | 32                       | 54    | 74         | 1.37                   |
| 11          | 330.3                   | 1.317         | 1.37              | 30                       | 59    | 80         | 1.36                   |
| 12          | 331.5                   | 1.301         | 1.44              | 33                       | 67    | 90         | 1.34                   |
| 13          | 332.7                   | 1.287         | 1.44              | 33                       | 68    | 93         | 1.37                   |
| 14          | 333.9                   | 1.273         | 1.18              | 23                       | 77    | 102        | 1.32                   |
| 15          | 335.2                   | 1.259         | 1.33              | 29                       | 81    | 105        | 1.30                   |
| 16          | 335.5                   | 1.246         | 1.39              | 31                       | 83    | 107        | 1.29                   |
| 17          | 337.8                   | 1.234         | 1.29              | 27                       | 91    | 111        | 1.22                   |
| 18          | 339.1                   | 1.222         | 0.92              | 9                        | 98    | 119        | 1.21                   |
| 19          | 340.5                   | 1.212         | 1.10              | 19                       | 101   | 118        | 1.17                   |
| 20          | 341.8                   | 1.202         | 1.21              | 24                       | 105   | 125        | 1.19                   |
| 21          | 40.0                    | 1.475         | 1.27              | 26                       | 22    | 36         | 1.64                   |
| 22          | 39.1                    | 1.456         | 1.04              | 17                       | 22    | 37         | 1.68                   |
| 23          | 38.1                    | 1.437         | 1.02              | 15                       | 25    | 40         | 1.60                   |
| 24          | 37.1                    | 1.418         | 1.07              | 18                       | 28    | 42         | 1.50                   |
| 25          | 36.1                    | 1.400         | 1.33              | 29                       | 31    | 42         | 1.35                   |
| 26          | 35.1                    | 1.383         | 1.40              | 31                       | 34    | 43         | 1.26                   |
| 27          | 34.0                    | 1.365         | 1.44              | 33                       | 39    | 48         | 1.23                   |
| 28          | 32.9                    | 1.349         | 1.21              | 24                       | 43    | 52         | 1.21                   |
| 29          | 31.8                    | 1.332         | 1.22              | 25                       | 48    | 62         | 1.29                   |
| 30          | 30.7                    | 1.317         | 1.20              | 24                       | 53    | 67         | 1.26                   |
| 31          | 29.5                    | 1.302         | 1.65              | 40                       | 57    | 72         | 1.26                   |
| 32          | 28.3                    | 1.287         | 1.55              | 36                       | 62    | 77         | 1.24                   |
| 33          | 27.1                    | 1.273         | 1.23              | 25                       | 74    | 85         | 1.15                   |
| 34          | 25.8                    | 1.259         | 1.09              | 19                       | 79    | 91         | 1.15                   |
| 35          | 24.5                    | 1.247         | 1.16              | 22                       | 85    | 100        | 1.18                   |

Table 1. Continued.

| No.          | Position<br>angle<br>$\theta$ | R/R<br>(3) <sup>o</sup> | FWHM<br>Å<br>(4) | $V_t$<br>kms <sup>-1</sup><br>(5) | $I_c$<br>(6) | $I_{max}$<br>(7) | $\frac{I_{max}}{I_c}$<br>(8) |
|--------------|-------------------------------|-------------------------|------------------|-----------------------------------|--------------|------------------|------------------------------|
| (1)          | (2)                           | (3)                     | (4)              | (5)                               | (6)          | (7)              | (8)                          |
| 36           | 23.2                          | 1.234                   | 1.46             | 33                                | 89           | 102              | 1.15                         |
| 37           | 21.9                          | 1.223                   | 1.18             | 23                                | 94           | 113              | 1.20                         |
| 38           | 20.5                          | 1.212                   | 1.36             | 30                                | 96           | 111              | 1.16                         |
| 39           | 19.2                          | 1.202                   | 1.35             | 29                                | 106          | 132              | 1.25                         |
| 40           | 17.8                          | 1.192                   | 1.04             | 17                                | 108          | 140              | 1.30                         |
| 41           | 15.6                          | 1.179                   | 1.47             | 34                                | 107          | 168              | 1.57                         |
| Slit IV (2)  |                               |                         |                  |                                   |              |                  |                              |
| 42           | 308.4                         | 1.403                   | 0.98             | 13                                | 21           | 26               | 1.24                         |
| 43           | 310.0                         | 1.355                   | 0.76             | 1                                 | 30           | 38               | 1.27                         |
| 44           | 312.6                         | 1.285                   | 0.96             | 12                                | 43           | 52               | 1.21                         |
| 45           | 313.5                         | 1.263                   | 1.28             | 27                                | 32           | 48               | 1.50                         |
| 46           | 314.5                         | 1.240                   | 1.39             | 31                                | 35           | 58               | 1.66                         |
| 47           | 315.5                         | 1.218                   | 1.34             | 29                                | 41           | 68               | 1.66                         |
| 48           | 316.5                         | 1.197                   | 1.45             | 33                                | 47           | 78               | 1.66                         |
| 49           | 318.2                         | 1.165                   | 1.23             | 25                                | 65           | 99               | 1.52                         |
| 50           | 319.9                         | 1.134                   | 0.67             | 0                                 | 90           | 207              | 2.30                         |
| 51           | 322.4                         | 1.096                   | 1.10             | 19                                | 116          | 299              | 2.58                         |
| 52           | 324.3                         | 1.068                   | 1.67             | 40                                | 148          | 407              | 2.75                         |
| 53           | 56.8                          | 1.553                   | 1.33             | 29                                | 10           | 13               | 1.30                         |
| 54           | 56.2                          | 1.528                   | 1.43             | 32                                | 12           | 16               | 1.33                         |
| 55           | 55.5                          | 1.502                   | 1.27             | 26                                | 12           | 17               | 1.42                         |
| 56           | 54.8                          | 1.477                   | 1.31             | 28                                | 16           | 23               | 1.44                         |
| 57           | 54.1                          | 1.452                   | 1.26             | 26                                | 19           | 27               | 1.42                         |
| 58           | 53.4                          | 1.428                   | 1.17             | 22                                | 22           | 33               | 1.50                         |
| 59           | 52.6                          | 1.403                   | 1.29             | 27                                | 20           | 44               | 2.20                         |
| 60           | 51.8                          | 1.379                   | 1.59             | 38                                | 26           | 48               | 1.85                         |
| 61           | 51.0                          | 1.355                   | 1.33             | 29                                | 28           | 53               | 1.89                         |
| 62           | 50.2                          | 1.332                   | 1.31             | 28                                | 35           | 57               | 1.63                         |
| 63           | 49.3                          | 1.308                   | 1.18             | 23                                | 41           | 67               | 1.63                         |
| 64           | 48.4                          | 1.285                   | 1.26             | 26                                | 50           | 73               | 1.46                         |
| 65           | 47.5                          | 1.263                   | 1.35             | 29                                | 57           | 77               | 1.35                         |
| 66           | 46.5                          | 1.240                   | 1.34             | 29                                | 71           | 89               | 1.25                         |
| 67           | 45.5                          | 1.218                   | 1.27             | 26                                | 77           | 87               | 1.13                         |
| 68           | 44.5                          | 1.197                   | 1.25             | 26                                | 86           | 98               | 1.14                         |
| 69           | 43.4                          | 1.176                   | 1.23             | 25                                | 96           | 112              | 1.17                         |
| 70           | 42.3                          | 1.155                   | 0.72             | 0                                 | 108          | 146              | 1.35                         |
| 71           | 41.1                          | 1.135                   | 1.02             | 15                                | 125          | 327              | 2.62                         |
| 72           | 39.9                          | 1.115                   | 1.42             | 32                                | 137          | 426              | 3.11                         |
| Slit III (1) |                               |                         |                  |                                   |              |                  |                              |
| 73           | 283.9                         | 1.660                   | 2.37             | 62                                | 8            | 11               | 1.38                         |
| 74           | 284.2                         | 1.623                   | 1.41             | 32                                | 10           | 13               | 1.30                         |
| 75           | 284.5                         | 1.586                   | 1.47             | 34                                | 10           | 13               | 1.30                         |
| 76           | 285.0                         | 1.541                   | 1.71             | 42                                | 14           | 20               | 1.43                         |
| 77           | 285.3                         | 1.511                   | 1.80             | 45                                | 14           | 21               | 1.50                         |
| 78           | 285.6                         | 1.481                   | 1.83             | 46                                | 17           | 24               | 1.41                         |
| 79           | 285.9                         | 1.452                   | 1.75             | 43                                | 21           | 31               | 1.48                         |
| 80           | 286.2                         | 1.422                   | 1.52             | 35                                | 28           | 43               | 1.54                         |
| 81           | 286.5                         | 1.393                   | 1.58             | 37                                | 35           | 51               | 1.46                         |
| 82           | 286.9                         | 1.363                   | 1.54             | 36                                | 41           | 65               | 1.59                         |
| 83           | 287.4                         | 1.326                   | 1.72             | 42                                | 53           | 81               | 1.53                         |
| 84           | 287.9                         | 1.289                   | 1.55             | 36                                | 71           | 104              | 1.46                         |
| 85           | 288.3                         | 1.260                   | 1.34             | 29                                | 85           | 140              | 1.65                         |

Table 1. Continued.

| No.          | position<br>angle<br>$\theta$ | $R/R_{\odot}$ | FWHM<br>Å | $V_r$<br>km s <sup>-1</sup> | $I_c$ | $I_{max}$ | $\frac{I_{max}}{I_c}$ |
|--------------|-------------------------------|---------------|-----------|-----------------------------|-------|-----------|-----------------------|
| (1)          | (2)                           | (3)           | (4)       | (5)                         | (6)   | (7)       | (8)                   |
| 86           | 76.3                          | 1.571         | 1.73      | 42                          | 8     | 12        | 1.50                  |
| 87           | 76.0                          | 1.541         | 1.42      | 32                          | 8     | 13        | 1.63                  |
| 88           | 75.8                          | 1.511         | 1.64      | 40                          | 9     | 16        | 1.78                  |
| 89           | 75.3                          | 1.467         | 1.65      | 40                          | 11    | 24        | 2.18                  |
| 90           | 75.0                          | 1.437         | 1.64      | 40                          | 13    | 34        | 2.62                  |
| 91           | 74.6                          | 1.407         | 1.72      | 42                          | 17    | 45        | 2.65                  |
| 92           | 74.1                          | 1.363         | 1.75      | 43                          | 22    | 62        | 2.82                  |
| 93           | 73.7                          | 1.334         | 1.93      | 49                          | 28    | 78        | 2.79                  |
| 94           | 73.3                          | 1.304         | 2.18      | 57                          | 34    | 89        | 2.62                  |
| 95           | 72.9                          | 1.275         | 2.32      | 61                          | 45    | 106       | 2.36                  |
| 96           | 72.5                          | 1.245         | 2.15      | 56                          | 57    | 127       | 2.23                  |
| 97           | 72.1                          | 1.216         | 2.12      | 55                          | 68    | 151       | 2.22                  |
| Slit III (2) |                               |               |           |                             |       |           |                       |
| 98           | 274.4                         | 1.573         | 1.10      | 19                          | 6     | 9         | 1.50                  |
| 99           | 274.5                         | 1.542         | 1.65      | 40                          | 6     | 10        | 1.67                  |
| 100          | 274.6                         | 1.511         | 1.47      | 34                          | 7     | 11        | 1.57                  |
| 101          | 274.7                         | 1.481         | 1.02      | 15                          | 9     | 13        | 1.44                  |
| 102          | 274.8                         | 1.450         | 1.45      | 33                          | 10    | 17        | 1.70                  |
| 103          | 274.9                         | 1.419         | 1.28      | 27                          | 12    | 22        | 1.83                  |
| 104          | 275.0                         | 1.389         | 1.31      | 28                          | 16    | 28        | 1.75                  |
| 105          | 275.1                         | 1.358         | 1.30      | 28                          | 22    | 36        | 1.64                  |
| 106          | 275.2                         | 1.327         | 1.52      | 35                          | 28    | 44        | 1.57                  |
| 107          | 275.3                         | 1.297         | 1.47      | 34                          | 35    | 55        | 1.57                  |
| 108          | 275.4                         | 1.266         | 1.25      | 26                          | 50    | 74        | 1.48                  |
| 109          | 275.5                         | 1.235         | 1.40      | 31                          | 71    | 90        | 1.27                  |
| 110          | 275.6                         | 1.205         | 1.38      | 30                          | 86    | 113       | 1.31                  |
| 111          | 275.8                         | 1.174         | 0.96      | 12                          | 106   | 202       | 1.91                  |
| 112          | 275.9                         | 1.143         | 1.57      | 37                          | 132   | 424       | 3.21                  |
| 113          | 87.0                          | 1.788         | 1.31      | 28                          | 5     | 8         | 1.60                  |
| 114          | 86.9                          | 1.711         | 0.74      | 1                           | 6     | 9         | 1.50                  |
| 115          | 86.7                          | 1.634         | 1.39      | 31                          | 7     | 10        | 1.43                  |
| 116          | 86.6                          | 1.604         | 0.96      | 12                          | 7     | 14        | 2.00                  |
| 117          | 86.6                          | 1.573         | 1.03      | 16                          | 9     | 16        | 1.78                  |
| 118          | 86.5                          | 1.542         | 1.39      | 31                          | 8     | 18        | 2.25                  |
| 119          | 86.4                          | 1.512         | 1.30      | 28                          | 10    | 25        | 2.50                  |
| 120          | 86.3                          | 1.481         | 1.24      | 25                          | 10    | 31        | 3.10                  |
| 121          | 86.2                          | 1.450         | 1.47      | 34                          | 12    | 38        | 3.17                  |
| 122          | 86.1                          | 1.419         | 1.45      | 33                          | 14    | 48        | 3.43                  |
| 123          | 86.0                          | 1.389         | 1.54      | 36                          | 19    | 65        | 3.42                  |
| 124          | 85.9                          | 1.358         | 1.68      | 41                          | 25    | 79        | 3.16                  |
| 125          | 85.8                          | 1.327         | 1.89      | 48                          | 36    | 92        | 2.56                  |
| 126          | 85.7                          | 1.297         | 1.94      | 49                          | 37    | 113       | 3.05                  |
| 127          | 85.6                          | 1.266         | 1.10      | 19                          | 56    | 200       | 3.57                  |
| 128          | 85.5                          | 1.235         | 1.01      | 15                          | 70    | 248       | 3.54                  |
| 129          | 85.4                          | 1.205         | 1.24      | 25                          | 93    | 492       | 5.29                  |
| 130          | 85.2                          | 1.174         | 1.27      | 26                          | 104   | 441       | 4.24                  |
| 131          | 85.1                          | 1.144         | 1.71      | 42                          | 124   | 452       | 3.65                  |
| Slit II (1)  |                               |               |           |                             |       |           |                       |
| 132          | 257.6                         | 1.657         | 1.92      | 48                          | 9     | 11        | 1.22                  |
| 133          | 257.3                         | 1.620         | 1.28      | 27                          | 9     | 10        | 1.11                  |
| 134          | 257.0                         | 1.582         | 1.79      | 44                          | 11    | 13        | 1.18                  |
| 135          | 256.6                         | 1.537         | 1.19      | 23                          | 13    | 17        | 1.31                  |
| 136          | 256.3                         | 1.507         | 1.56      | 37                          | 14    | 19        | 1.36                  |

Table 1. Continued.

| No.         | Position<br>angle<br>$\theta$ | $R/R_{\odot}$ | FWHM<br>Å | $V_r$<br>km s <sup>-1</sup> | $I_c$ | $I_{max}$ | $\frac{I_{max}}{I_c}$ |
|-------------|-------------------------------|---------------|-----------|-----------------------------|-------|-----------|-----------------------|
| (1)         | (2)                           | (3)           | (4)       | (5)                         | (6)   | (7)       | (8)                   |
| 137         | 256.0                         | 1.478         | 1.62      | 39                          | 18    | 22        | 1.22                  |
| 138         | 255.7                         | 1.448         | 2.00      | 51                          | 21    | 26        | 1.24                  |
| 139         | 255.4                         | 1.418         | 1.81      | 45                          | 31    | 38        | 1.23                  |
| 140         | 255.1                         | 1.388         | 1.88      | 47                          | 39    | 46        | 1.18                  |
| 141         | 254.7                         | 1.359         | 1.81      | 45                          | 52    | 60        | 1.15                  |
| 142         | 254.3                         | 1.322         | 1.65      | 40                          | 72    | 79        | 1.10                  |
| 143         | 253.8                         | 1.285         | 1.51      | 35                          | 93    | 100       | 1.08                  |
| 144         | 253.4                         | 1.255         | 1.24      | 25                          | 110   | 125       | 1.14                  |
| 145         | 104.1                         | 1.567         | 1.94      | 49                          | 12    | 15        | 1.25                  |
| 146         | 104.4                         | 1.537         | 20.6      | 53                          | 12    | 14        | 1.17                  |
| 147         | 104.7                         | 1.507         | 1.88      | 47                          | 13    | 16        | 1.23                  |
| 148         | 105.1                         | 1.463         | 2.17      | 56                          | 14    | 19        | 13.6                  |
| 149         | 105.4                         | 1.433         | 2.09      | 54                          | 18    | 22        | 1.22                  |
| 150         | 105.8                         | 1.403         | 2.23      | 58                          | 21    | 25        | 1.19                  |
| 151         | 106.3                         | 1.359         | 2.33      | 61                          | 25    | 29        | 1.16                  |
| 152         | 106.6                         | 1.329         | 2.40      | 63                          | 29    | 24        | 1.17                  |
| 153         | 107.0                         | 1.300         | 1.76      | 43                          | 34    | 40        | 1.17                  |
| 154         | 107.4                         | 1.270         | 1.48      | 34                          | 43    | 50        | 1.16                  |
| 155         | 107.8                         | 1.241         | 1.65      | 40                          | 49    | 55        | 1.12                  |
| 156         | 108.2                         | 1.211         | 1.67      | 41                          | 57    | 62        | 1.19                  |
| 157         | 108.7                         | 1.182         | 1.73      | 42                          | 72    | 78        | 1.08                  |
| 158         | 109.2                         | 1.153         | 1.75      | 43                          | 76    | 82        | 1.08                  |
| 159         | 109.9                         | 1.109         | 1.21      | 24                          | 91    | 108       | 1.19                  |
| Slit II (2) |                               |               |           |                             |       |           |                       |
| 160         | 248.1                         | 1.697         | 1.94      | 49                          | 5     | 8         | 1.60                  |
| 161         | 247.7                         | 1.669         | 1.32      | 28                          | 6     | 9         | 1.50                  |
| 162         | 247.3                         | 1.640         | 2.09      | 54                          | 6     | 9         | 1.50                  |
| 163         | 246.9                         | 1.612         | 1.72      | 42                          | 6     | 10        | 1.67                  |
| 164         | 246.4                         | 1.584         | 1.35      | 29                          | 8     | 12        | 1.50                  |
| 165         | 246.0                         | 1.556         | 1.17      | 22                          | 9     | 15        | 1.67                  |
| 166         | 245.5                         | 1.528         | 1.32      | 28                          | 10    | 19        | 1.90                  |
| 167         | 245.0                         | 1.500         | 1.65      | 40                          | 11    | 24        | 2.18                  |
| 168         | 244.5                         | 1.472         | 1.90      | 48                          | 13    | 31        | 2.38                  |
| 169         | 242.8                         | 1.363         | 1.91      | 48                          | 28    | 77        | 2.75                  |
| 170         | 241.6                         | 1.336         | 1.44      | 33                          | 46    | 92        | 2.00                  |
| 171         | 240.9                         | 1.309         | 1.50      | 35                          | 58    | 103       | 1.78                  |
| 172         | 240.3                         | 1.282         | 1.34      | 29                          | 75    | 126       | 1.68                  |
| 173         | 238.8                         | 1.230         | 1.13      | 21                          | 104   | 333       | 3.20                  |
| 174         | 115.5                         | 1.528         | 0.68      | 0                           | 9     | 15        | 1.67                  |
| 175         | 116.0                         | 1.500         | 1.20      | 24                          | 11    | 19        | 1.73                  |
| 176         | 116.5                         | 1.472         | 1.55      | 36                          | 11    | 18        | 1.64                  |
| 177         | 117.0                         | 1.445         | 1.52      | 35                          | 12    | 21        | 1.75                  |
| 178         | 117.6                         | 1.417         | 1.68      | 41                          | 14    | 28        | 2.00                  |
| 179         | 118.2                         | 1.390         | 1.88      | 47                          | 16    | 33        | 2.06                  |
| 180         | 118.8                         | 1.363         | 1.70      | 41                          | 23    | 43        | 1.87                  |
| 181         | 119.4                         | 1.336         | 1.57      | 37                          | 27    | 47        | 1.74                  |
| 182         | 120.1                         | 1.309         | 1.71      | 42                          | 31    | 54        | 1.74                  |
| 183         | 120.8                         | 1.282         | 1.51      | 35                          | 42    | 63        | 1.50                  |
| 184         | 121.5                         | 1.256         | 1.52      | 35                          | 51    | 71        | 1.39                  |
| 185         | 122.2                         | 1.230         | 1.17      | 22                          | 64    | 79        | 1.23                  |
| 186         | 123.0                         | 1.203         | 1.27      | 26                          | 77    | 84        | 1.09                  |
| 187         | 123.8                         | 1.178         | 1.43      | 32                          | 85    | 96        | 1.13                  |
| 188         | 124.6                         | 1.152         | 0.69      | 0                           | 99    | 114       | 1.15                  |
| 189         | 125.5                         | 1.127         | 1.10      | 19                          | 104   | 127       | 1.22                  |
| 190         | 126.4                         | 1.102         | 1.38      | 31                          | 132   | 256       | 1.94                  |



Table 1. Concluded.

| No.        | Position<br>angle<br>$\theta$ | $R/R_{\odot}$ | FWHM<br>Å | $V_t$<br>km s <sup>-1</sup> | $I_c$ | $I_{max}$ | $\frac{I_{max}}{I_c}$ |
|------------|-------------------------------|---------------|-----------|-----------------------------|-------|-----------|-----------------------|
| (1)        | (2)                           | (3)           | (4)       | (5)                         | (6)   | (7)       | (8)                   |
| Slit I (1) |                               |               |           |                             |       |           |                       |
| 191        | 218.5                         | 1.425         | 2.05      | 53                          | 40    | 46        | 1.15                  |
| 192        | 217.5                         | 1.406         | 2.03      | 52                          | 42    | 48        | 1.14                  |
| 193        | 216.5                         | 1.388         | 1.91      | 48                          | 48    | 55        | 1.15                  |
| 194        | 215.4                         | 1.370         | 2.06      | 53                          | 49    | 55        | 1.12                  |
| 195        | 214.4                         | 1.353         | 1.21      | 24                          | 53    | 58        | 1.09                  |
| 196        | 213.3                         | 1.336         | 1.64      | 40                          | 53    | 58        | 1.09                  |
| 197        | 212.2                         | 1.319         | 2.04      | 52                          | 57    | 61        | 1.07                  |
| 198        | 209.2                         | 1.281         | 1.18      | 23                          | 66    | 68        | 1.03                  |
| 199        | 146.1                         | 1.361         | 1.54      | 36                          | 17    | 21        | 1.24                  |
| 200        | 148.8                         | 1.319         | 2.21      | 58                          | 20    | 25        | 1.25                  |
| 201        | 151.8                         | 1.280         | 2.14      | 55                          | 26    | 30        | 1.15                  |
| 202        | 154.9                         | 1.245         | 2.10      | 54                          | 32    | 41        | 1.28                  |
| 203        | 158.2                         | 1.214         | 2.32      | 61                          | 47    | 54        | 1.15                  |
| 204        | 161.6                         | 1.187         | 1.71      | 42                          | 62    | 68        | 1.10                  |
| 205        | 168.9                         | 1.147         | 1.52      | 35                          | 93    | 100       | 1.08                  |
| Slit I (2) |                               |               |           |                             |       |           |                       |
| 206        | 213.9                         | 1.677         | 1.35      | 29                          | 12    | 17        | 1.42                  |
| 207        | 213.0                         | 1.660         | 0.72      | 0                           | 12    | 18        | 1.50                  |
| 208        | 212.1                         | 1.644         | 1.23      | 25                          | 12    | 17        | 1.42                  |
| 209        | 211.2                         | 1.628         | 1.61      | 39                          | 12    | 16        | 1.33                  |
| 210        | 209.8                         | 1.605         | 1.44      | 33                          | 13    | 19        | 1.46                  |
| 211        | 208.3                         | 1.583         | 1.42      | 32                          | 15    | 22        | 1.47                  |
| 212        | 206.3                         | 1.555         | 1.45      | 33                          | 16    | 25        | 1.56                  |
| 213        | 204.8                         | 1.535         | 1.28      | 27                          | 19    | 26        | 1.37                  |
| 214        | 203.2                         | 1.517         | 1.56      | 37                          | 21    | 28        | 1.33                  |
| 215        | 201.0                         | 1.495         | 1.31      | 28                          | 24    | 28        | 1.17                  |
| 216        | 199.3                         | 1.479         | 1.10      | 19                          | 26    | 32        | 1.23                  |
| 217        | 197.6                         | 1.465         | 1.32      | 28                          | 29    | 36        | 1.24                  |
| 218        | 195.3                         | 1.448         | 1.74      | 43                          | 30    | 38        | 1.27                  |
| 219        | 193.5                         | 1.437         | 1.25      | 26                          | 34    | 38        | 1.12                  |
| 220        | 191.7                         | 1.427         | 1.54      | 36                          | 34    | 40        | 1.18                  |
| 221        | 189.3                         | 1.416         | 1.72      | 42                          | 35    | 41        | 1.17                  |
| 222        | 187.4                         | 1.410         | 1.20      | 24                          | 38    | 41        | 1.08                  |
| 223        | 185.5                         | 1.405         | 1.03      | 16                          | 42    | 45        | 1.07                  |
| 224        | 183.0                         | 1.401         | 1.10      | 19                          | 43    | 54        | 1.26                  |
| 225        | 181.1                         | 1.400         | 1.28      | 27                          | 42    | 50        | 1.19                  |
| 226        | 156.3                         | 1.536         | 1.13      | 21                          | 9     | 10        | 1.11                  |
| 227        | 158.9                         | 1.506         | 1.33      | 29                          | 10    | 13        | 1.30                  |
| 228        | 161.1                         | 1.484         | 1.72      | 42                          | 12    | 16        | 1.33                  |
| 229        | 162.8                         | 1.469         | 1.23      | 25                          | 15    | 20        | 1.33                  |
| 230        | 164.6                         | 1.456         | 1.68      | 41                          | 18    | 23        | 1.28                  |
| 231        | 166.9                         | 1.440         | 1.36      | 30                          | 24    | 32        | 1.33                  |
| 232        | 168.7                         | 1.430         | 1.45      | 33                          | 28    | 36        | 1.29                  |
| 233        | 170.5                         | 1.421         | 1.93      | 49                          | 31    | 38        | 1.23                  |
| 234        | 172.4                         | 1.414         | 1.23      | 25                          | 31    | 40        | 1.29                  |
| 235        | 174.2                         | 1.408         | 1.52      | 35                          | 31    | 39        | 1.26                  |
| 236        | 179.2                         | 1.400         | 0.96      | 12                          | 38    | 42        | 1.11                  |

## 4.1 Line Widths

The derived values of FWHM of the red coronal line varies between  $0.6\text{\AA}$  and  $2.4\text{\AA}$ . The values at the different locations are depicted in Fig. 3. One can thus evaluate the association of any line widening with coronal form. When we plot a histogram of line-width dependence, as in Fig. 4, we find a predominance of values of FWHM

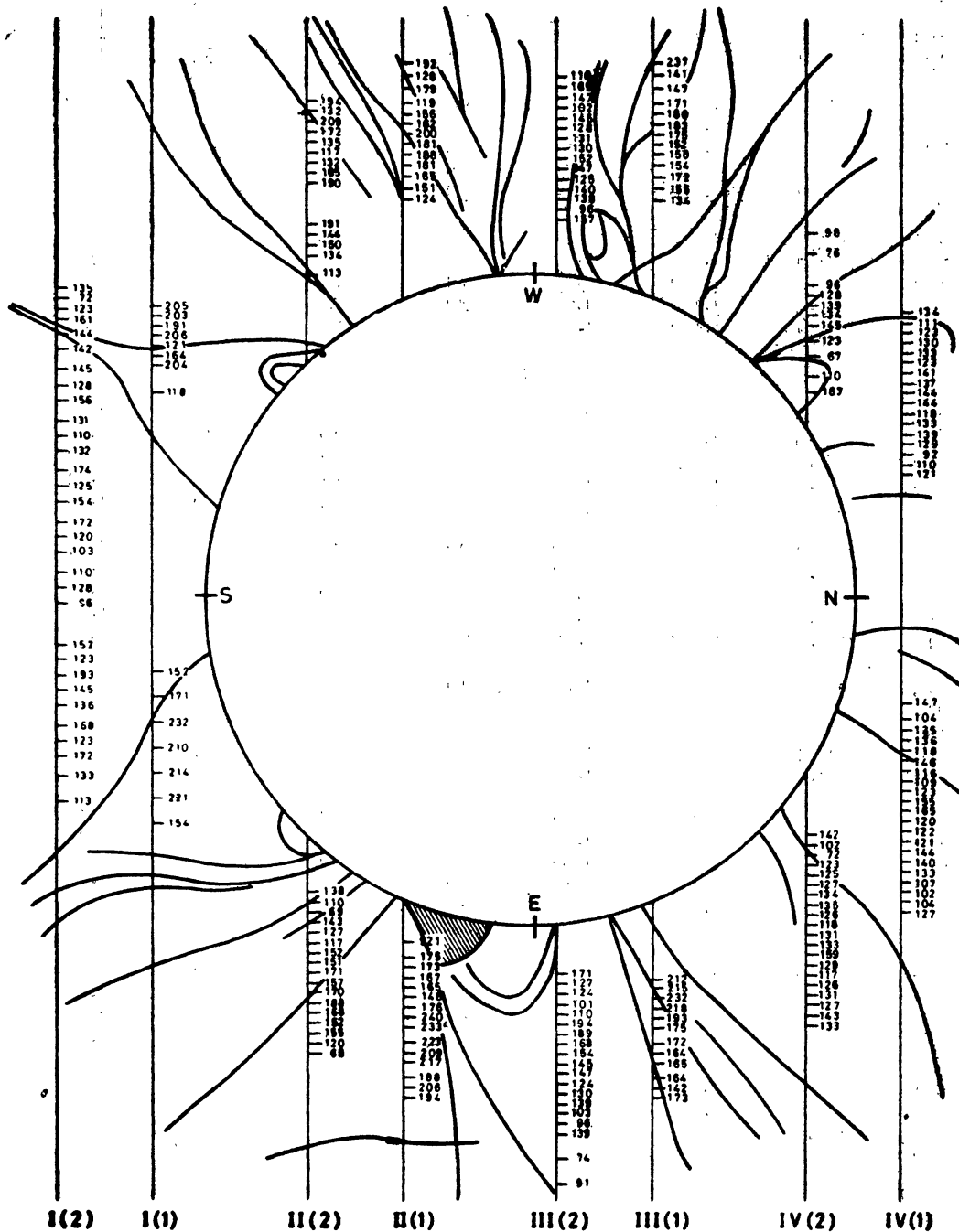


Figure 3. True line widths of  $[\text{Fe x}] 6374\text{\AA}$  line are written at various locations in  $\text{\AA} \times 10^{-2}$ . I(1), II(1), III(1) and IV(1) are the slit positions on solar disc with plate 1 and correspondingly with suffix 2 in bracket are due to plate 2. A sketch of white-light corona is super-imposed to compare the two. Shaded area on E-limb is an enhancement observed in white light corona and the horizontal line crossing slit positions II(2) and II(1) is the filament.

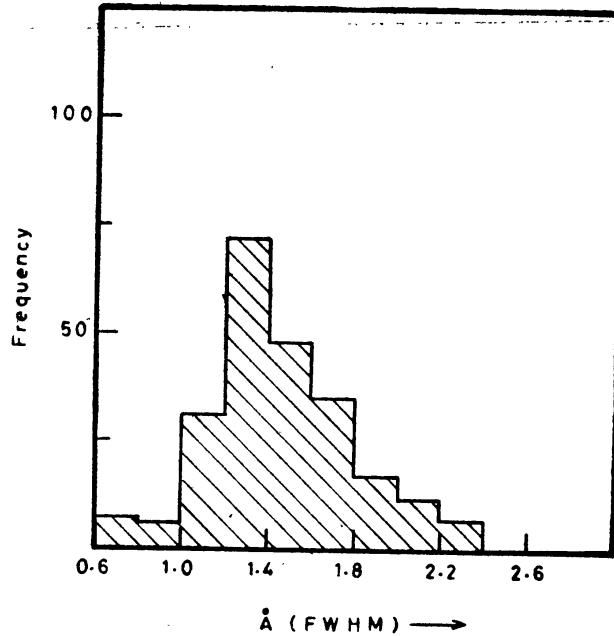


Figure 4. Frequency distribution of true line widths of [Fe x] 6374 Å.

around 1.3 Å and an extended tail towards larger values. The lowest value of line width is 0.6 Å. If thermal broadening is the only contributor to line widths then with the aid of the standard kinetic-temperature formula one derives a temperature of  $1.2 \times 10^6$  K for a line width of 0.67 Å. The temperature assumes higher values, if one converts the peak of the FWHM of 1.3 Å. The value is then  $4.6 \times 10^6$  K while the largest value of line width of 2.4 Å represents even a higher value of temperature, if one interprets it to be so. Jordan (1969) had calculated the ionization equilibrium as a function of temperature for several of the ions commonly seen in eclipse spectra. Fe x is mostly available in the temperature zone  $5 \times 10^5$ – $2 \times 10^6$ , with a peak at  $1.3 \times 10^6$  K. It therefore becomes inadmissible to accept the high values of temperature inferred from line widths, especially for a relatively low temperature ion like Fe x. Therefore the need to assume an additional line-broadening agency seems necessary. Introducing a turbulence parameter in the equation, and assuming the ions of iron to be controlled by the peak value of  $1.3 \times 10^6$  K (Jordan 1969), one finds turbulent velocities of  $30 \text{ km s}^{-1}$  from line broadening. The smallest values in the histogram of line widths seems to be representative of the state of ionization. The larger FWHM must necessarily signify the appreciable contribution to it by Doppler motion. An evaluation of this characteristic is extremely difficult. For, in the line of sight of an optically thin gas, we witness—besides the effects of thermal broadening—several other factors. The presence of broadening by random motions is clear. The value of  $30 \text{ km s}^{-1}$  is in good accord with that derived by Delone and Makarova (1969). The advantages of similar studies at future eclipses, based on simultaneous exposures of lines of at least two different atomic weights, are obvious.

#### 4.2 Line and Continuum Intensities

Our measures of intensity, both at the peak of the line and at the underlying continuum, can be used for the study of gradients of both the emission corona and the K corona.

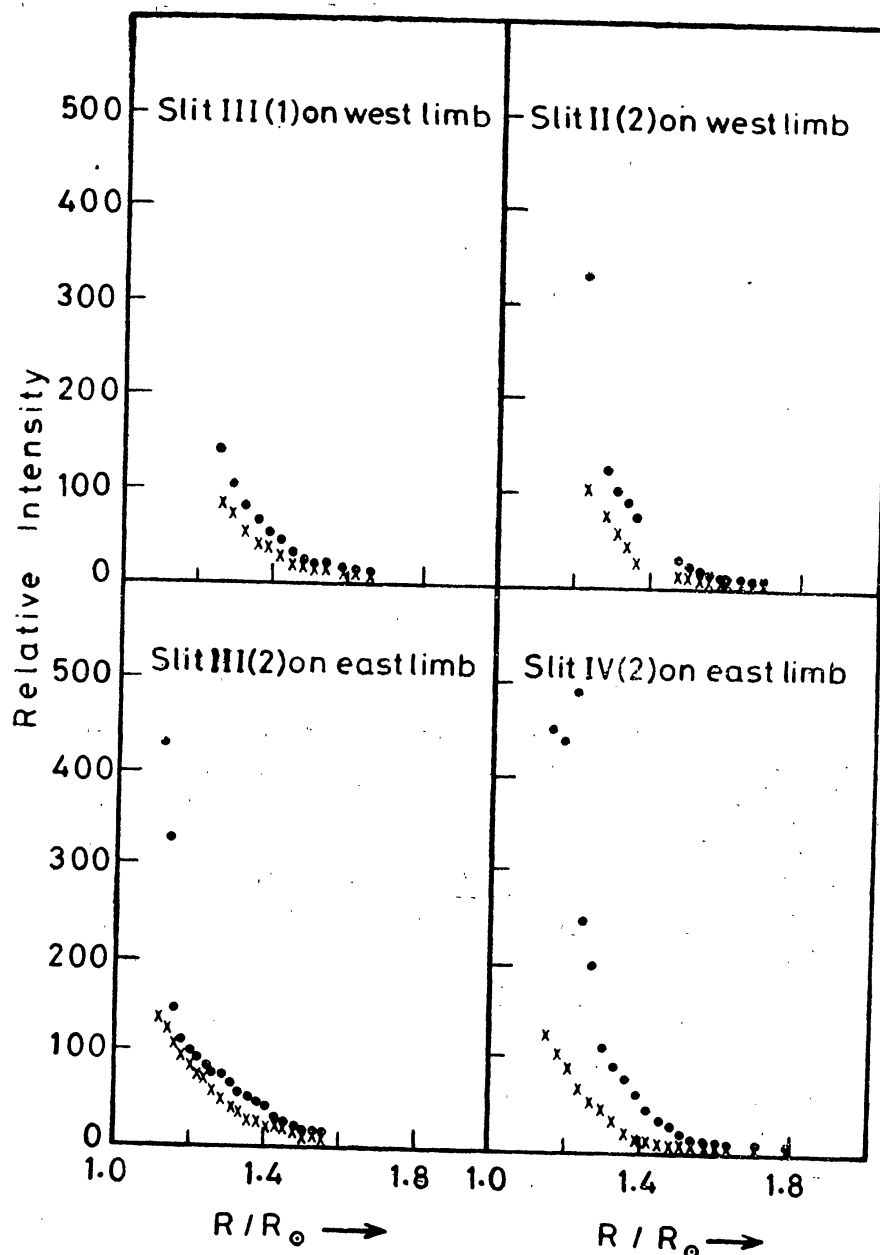


Figure 5. A plot of continuum (crosses) and the [Fe x] line (filled circles) intensity versus radial distance.

The multislit arrangement covers several helmets and streamers and it is possible to choose those locations where the slit has an almost radial orientation. When we do this for the K corona along the locations (a) western part of slits II (2) and III (1) and (b) eastern part of slits III (2) and IV (2) as indicated in Fig. 3, we obtain gradients of intensity shown in Fig. 5 consistent with the trends known to exist in such features over a century of observing eclipses. Coronal emission-line intensities are the straight ratios of Column (8) in Table 1. These conform to the steep gradients of emission lines that we are familiar with. A logarithmic representation is seen in Fig. 6.

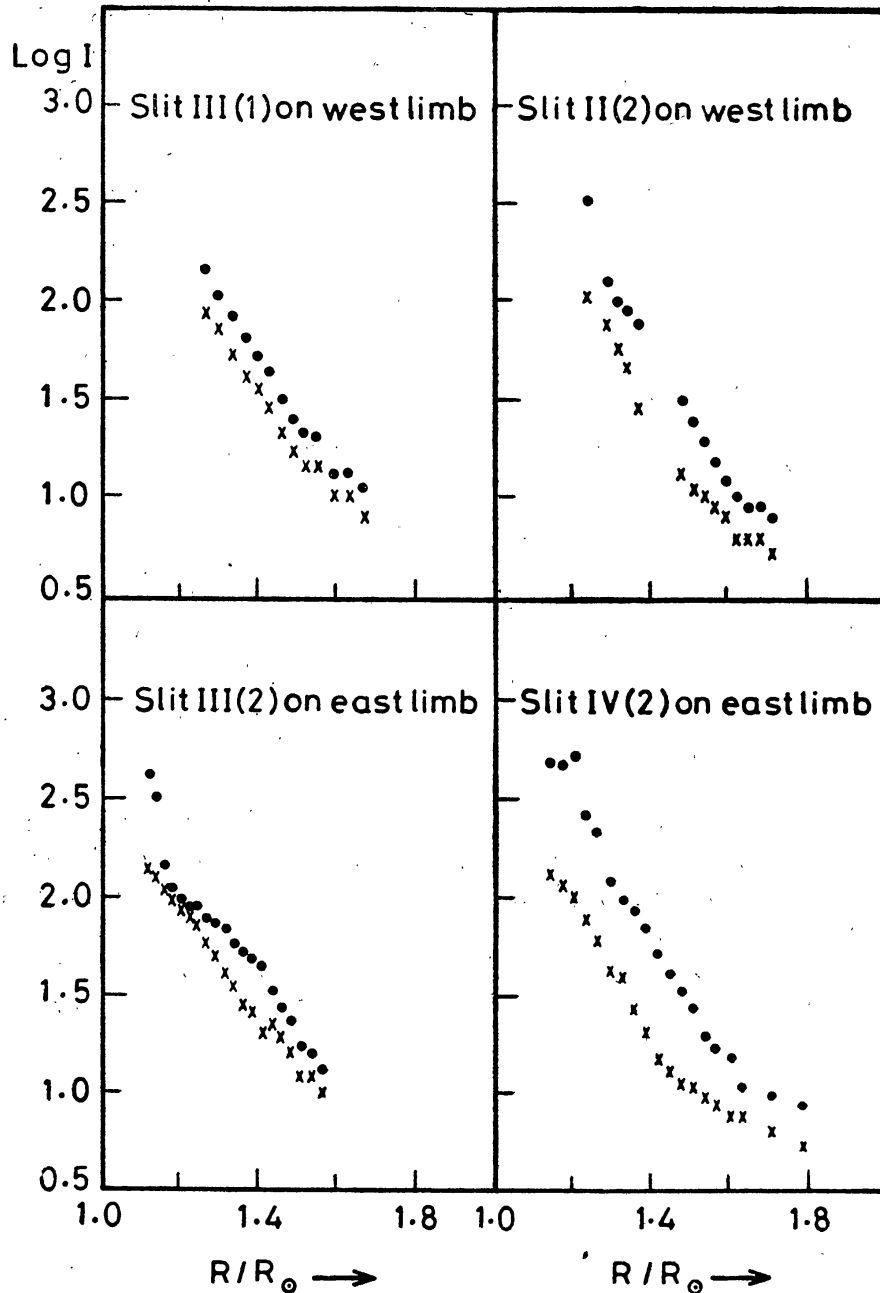


Figure 6. Logarithmic intensity of continuum (crosses) and the [Fe x] line (filled circles) versus radial distance.

#### 4.3 Coronal Hole and Transient

A noticeable coronal hole near the south pole was one of the striking features of the 1980 eclipse. We have several measures that cover the position angle range  $170^{\circ}$ – $190^{\circ}$ . The tangential slit position restricts the  $R/R_{\odot}$  values from 1.43 to 1.53. A noticeable characteristic of the line widths is that a majority of them have small values. We interpret this to mean that the random motions sampled in this region in the line of sight are of small magnitude, a picture consistent with the open field structure and guided radial plasma outflow over a coronal hole.

Coronal transients are normally rare events to be observed during an eclipse. Such features were observed above the west limb by Japanese observers among others located in Kenya. The region had quietened down by the time moon's shadow had reached India. There is an enhancement near the limb in the white light corona at position angle  $106^\circ$  seen by several teams. K. K. Scaria of Indian Institute of Astrophysics, who obtained high-resolution white-light pictures of the sun in India, reports a filament structure in the position angle range  $95^\circ$  to  $118^\circ$  and at a mean distance of  $1.73 R_\odot$ . This filament seems to be remnant of a transient display. The region near the limb continued to be highly disturbed; the highest values of line width of the red line measured anywhere in the corona are found in this region even to large values of  $R_\odot$ .

#### 4.4 Line-of-Sight Velocities in the Corona and Coronal Equatorial Rotation

We have measured radial velocities with the aid of the neon comparison lines, at several points along each slit on both the east and west corona. These values are shown in Table 2 and refer to the solar equator. In particular, slit positions II (1), III (2) and III (1) have been utilized for the rotation measures. The differences amongst the several different values of displacement of the coronal emission line lowers the accuracy of measurement; this is unlike the measures from absorption lines of photospheric origin. We have therefore grouped for each slit position, the east and west values. The mean wavelength of the line is derived from the measures near the north and south poles of the sun. The coronal rotation is thus  $2.6 \text{ km s}^{-1}$  and is comparable to the photospheric value. The limited accuracy of our measures (probable error  $\pm 1.5 \text{ km s}^{-1}$ ) of faint broad lines only permits a confirmation of co-rotation of the corona.

A distribution of line-of-sight velocities measured all over the corona is displayed in Fig. 7. None of the regions covered by our multislit arrangement show abnormally

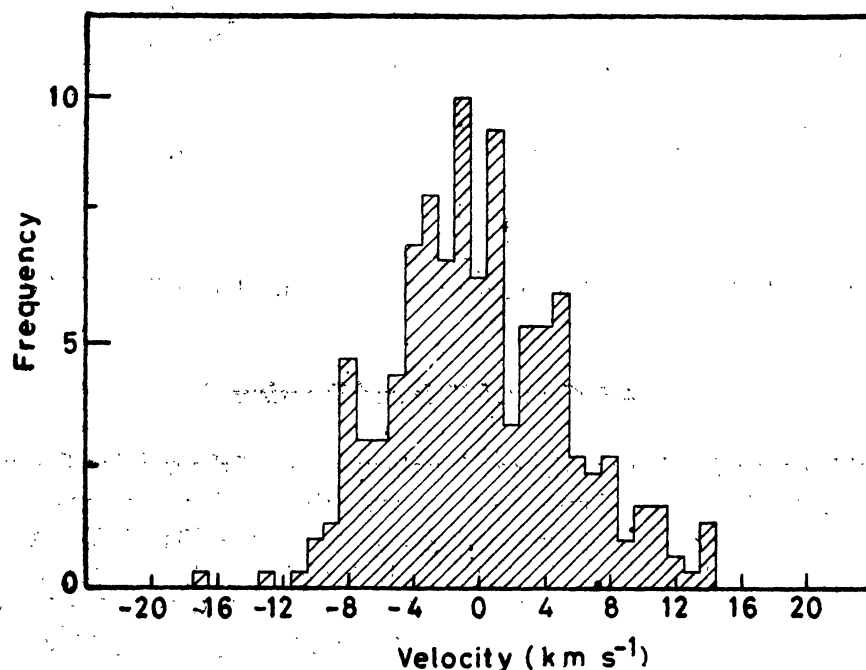


Figure 7. Frequency distribution of line-of-sight velocities as derived from [Fe x] 6374Å line.

large velocities in the corona reported earlier by Delone and Makarova (1969) and for this eclipse by Chandrasekhar, Desai and Angreji (1981). The latter find a splitting of the interference fringe pattern at position angle  $256^\circ$  indicating a component with a line-of-sight velocity of  $70 \text{ km s}^{-1}$ . This would imply, if confirmed, that there is a mass component with a velocity indicating expansion in perhaps a preferred direction. This region is covered by our slit position II (1), that spans the position angle  $252^\circ$ – $257^\circ$ . Not only do we not see any splitting of the emission line, but we also do not find any abnormal shift even of the line as a whole. The observed velocities are all within the range  $\pm 11 \text{ km s}^{-1}$ . However, one should note that we have derived the line-of-sight velocities from the red coronal line sensitive to a region with temperature of  $1.3 \times 10^6 \text{ K}$  whereas Chandrasekhar, Desai and Angreji (1981) have measured from the green line contributed mostly from regions with a temperature of  $2.5 \times 10^6 \text{ K}$ .

Table 2. Line-of-sight velocities derived from the red coronal line.

| No.         | Position angle | $R/R_\odot$ | $v$<br>$\text{km s}^{-1}$ | No. | Position angle | $R/R_\odot$ | $v$<br>$\text{km s}^{-1}$ |
|-------------|----------------|-------------|---------------------------|-----|----------------|-------------|---------------------------|
| (1)         | (2)            | (3)         | (4)                       | (1) | (2)            | (3)         | (4)                       |
| Slit IV (1) |                |             |                           | 36  | 7.4            | 1.151       | 8                         |
|             |                |             |                           | 37  | 9.0            | 1.156       | 2                         |
| 1           | 320.1          | 1.495       | 1                         | 38  | 10.0           | 1.162       | -1                        |
| 2           | 321.0          | 1.475       | 1                         | 39  | 12.0           | 1.168       | 2                         |
| 3           | 321.9          | 1.456       | 1                         | 40  | 13.4           | 1.175       | 5                         |
| 4           | 322.9          | 1.437       | 0                         |     |                |             |                           |
| 5           | 323.9          | 1.418       | -5                        | 41  | 14.9           | 1.183       | 3                         |
|             |                |             |                           | 42  | 16.3           | 1.192       | 5                         |
| 6           | 324.9          | 1.400       | -6                        | 43  | 17.8           | 1.202       | 3                         |
| 7           | 325.9          | 1.383       | -1                        | 44  | 19.2           | 1.212       | -1                        |
| 8           | 327.0          | 1.365       | -2                        | 45  | 20.5           | 1.223       | 1                         |
| 9           | 328.1          | 1.348       | 0                         |     |                |             |                           |
| 10          | 329.2          | 1.332       | 1                         | 46  | 21.9           | 1.234       | 1                         |
|             |                |             |                           | 47  | 23.2           | 1.247       | -2                        |
| 11          | 330.3          | 1.317       | -7                        | 48  | 24.5           | 1.259       | -2                        |
| 12          | 331.5          | 1.301       | -3                        | 49  | 25.8           | 1.273       | -2                        |
| 13          | 332.7          | 1.287       | 3                         | 50  | 27.1           | 1.287       | -7                        |
| 14          | 333.9          | 1.273       | -1                        |     |                |             |                           |
| 15          | 335.2          | 1.259       | 0                         | 51  | 28.3           | 1.302       | -2                        |
|             |                |             |                           | 52  | 29.5           | 1.317       | -3                        |
| 16          | 336.5          | 1.247       | -1                        | 53  | 30.7           | 1.332       | -1                        |
| 17          | 337.8          | 1.234       | 2                         | 54  | 31.8           | 1.349       | -4                        |
| 18          | 339.1          | 1.223       | 1                         | 55  | 32.9           | 1.365       | -8                        |
| 19          | 340.5          | 1.219       | -1                        |     |                |             |                           |
| 20          | 341.8          | 1.202       | -1                        | 56  | 34.0           | 1.383       | 1                         |
|             |                |             |                           | 57  | 35.1           | 1.400       | -6                        |
| 21          | 343.2          | 1.192       | 0                         | 58  | 36.1           | 1.418       | -4                        |
| 22          | 344.7          | 1.183       | 1                         | 59  | 37.1           | 1.437       | -1                        |
| 23          | 346.1          | 1.175       | -2                        | 60  | 38.1           | 1.456       | -1                        |
| 24          | 349.1          | 1.162       | 4                         |     |                |             |                           |
| 25          | 350.5          | 1.156       | 8                         | 61  | 40.0           | 1.475       | -8                        |
|             |                |             |                           | 62  | 40.9           | 1.495       | -5                        |
| 26          | 352.0          | 1.151       | 5                         | 63  | 41.8           | 1.515       | -3                        |
| 27          | 353.6          | 1.147       | 5                         | 64  | 42.7           | 1.536       | -8                        |
| 28          | 355.1          | 1.144       | 11                        | 65  | 43.5           | 1.557       | -3                        |
| 29          | 356.6          | 1.141       | 7                         |     |                |             |                           |
| 30          | 358.2          | 1.139       | 4                         | 66  | 44.3           | 1.578       | -6                        |
|             |                |             |                           | 67  | 45.1           | 1.599       | -10                       |
| 31          | 359.7          | 1.139       | 3                         | 68  | 45.9           | 1.621       | -3                        |
| 32          | 1.3            | 1.139       | 2                         | 69  | 46.6           | 1.643       | -8                        |
| 33          | 2.8            | 1.141       | 3                         | 70  | 47.3           | 1.665       | -9                        |
| 34          | 4.4            | 1.143       | 4                         |     |                |             |                           |
| 35          | 5.9            | 1.147       | 0                         |     |                |             |                           |

Table 2. Continued.

| No.          | Position angle | $R/R_{\odot}$ | $v$<br>km s <sup>-1</sup> | No.          | Position angle | $R/R_{\odot}$ | $v$<br>km s <sup>-1</sup> |
|--------------|----------------|---------------|---------------------------|--------------|----------------|---------------|---------------------------|
| (1)          | (2)            | (3)           | (4)                       | (1)          | (2)            | (3)           | (4)                       |
| Slit IV (2)  |                |               |                           | 121          | 74.8           | 1.422         | -6                        |
| 71           | 312.1          | 1.297         | 0                         | 122          | 74.5           | 1.393         | -4                        |
| 72           | 313.1          | 1.274         | -1                        | 123          | 74.1           | 1.363         | -2                        |
| 73           | 314.0          | 1.251         | 1                         | 124          | 73.7           | 1.334         | -5                        |
| 74           | 315.0          | 1.229         | 2                         | 125          | 73.3           | 1.304         | -4                        |
| 75           | 316.0          | 1.207         | 3                         | 126          | 72.9           | 1.275         | -7                        |
| 76           | 317.1          | 1.186         | 5                         | 127          | 72.5           | 1.245         | -3                        |
| 77           | 318.2          | 1.165         | 5                         | 128          | 72.1           | 1.216         | -6                        |
| 78           | 319.3          | 1.145         | 10                        | 129          | 71.6           | 1.187         | 0                         |
| 79           | 320.5          | 1.125         | 10                        | 130          | 71.1           | 1.158         | 1                         |
| 80           | 53.8           | 1.440         | -7                        | Slit III (2) |                |               |                           |
| 81           | 53.0           | 1.415         | -2                        | 131          | 274.6          | 1.496         | -1                        |
| 82           | 52.2           | 1.391         | -2                        | 132          | 274.7          | 1.465         | -3                        |
| 83           | 51.4           | 1.367         | -1                        | 133          | 274.8          | 1.435         | -2                        |
| 84           | 50.6           | 1.343         | 0                         | 134          | 274.9          | 1.404         | 0                         |
| 85           | 49.8           | 1.320         | -4                        | 135          | 275.0          | 1.373         | -1                        |
| 86           | 48.9           | 1.297         | -3                        | 136          | 275.1          | 1.343         | 1                         |
| 87           | 48.0           | 1.274         | -1                        | 137          | 275.2          | 1.312         | 4                         |
| 88           | 47.0           | 1.251         | -4                        | 138          | 275.3          | 1.281         | 6                         |
| 89           | 46.0           | 1.229         | -3                        | 139          | 275.4          | 1.251         | 5                         |
| 90           | 45.0           | 1.208         | -3                        | 140          | 275.6          | 1.220         | 5                         |
| 91           | 43.9           | 1.186         | -5                        | 141          | 275.7          | 1.189         | 4                         |
| 92           | 42.8           | 1.165         | 0                         | 142          | 86.7           | 1.619         | 0                         |
| 93           | 41.7           | 1.145         | -1                        | 143          | 86.6           | 1.588         | -2                        |
| Slit III (1) |                |               |                           | 144          | 86.5           | 1.557         | -2                        |
| 94           | 284.2          | 1.631         | 1                         | 145          | 86.5           | 1.527         | -5                        |
| 95           | 284.4          | 1.600         | -4                        | 146          | 86.4           | 1.496         | -3                        |
| 96           | 284.7          | 1.571         | -10                       | 147          | 86.3           | 1.465         | -5                        |
| 97           | 285.0          | 1.541         | -2                        | 148          | 86.2           | 1.435         | -8                        |
| 98           | 285.3          | 1.511         | 0                         | 149          | 86.1           | 1.404         | -8                        |
| 99           | 285.6          | 1.482         | -3                        | 150          | 86.0           | 1.373         | -8                        |
| 100          | 285.9          | 1.452         | -4                        | 151          | 85.9           | 1.342         | -4                        |
| 101          | 286.2          | 1.422         | -4                        | 152          | 85.8           | 1.312         | -3                        |
| 102          | 286.5          | 1.392         | 1                         | 153          | 85.7           | 1.281         | -2                        |
| 103          | 286.9          | 1.363         | 0                         | 154          | 85.6           | 1.251         | -2                        |
| 104          | 287.3          | 1.333         | -1                        | 155          | 85.4           | 1.220         | -4                        |
| 105          | 287.7          | 1.304         | 5                         | 156          | 85.3           | 1.189         | -3                        |
| 106          | 288.1          | 1.275         | 4                         | 157          | 85.2           | 1.159         | -4                        |
| 107          | 288.5          | 1.245         | 9                         | 158          | 85.0           | 1.128         | -4                        |
| 108          | 289.0          | 1.216         | -1                        | Slit II (1)  |                |               |                           |
| 109          | 289.4          | 1.187         | 11                        | 159          | 256.3          | 1.507         | 11                        |
| 110          | 289.9          | 1.158         | 10                        | 160          | 256.0          | 1.477         | 6                         |
| 111          | 290.4          | 1.129         | 14                        | 161          | 255.7          | 1.448         | 9                         |
| 112          | 77.3           | 1.690         | 3                         | 162          | 255.4          | 1.418         | 1                         |
| 113          | 77.1           | 1.660         | -4                        | 163          | 255.1          | 1.388         | 3                         |
| 114          | 76.9           | 1.631         | -7                        | 164          | 254.7          | 1.359         | 0                         |
| 115          | 76.6           | 1.601         | -5                        | 165          | 254.4          | 1.329         | 1                         |
| 116          | 76.3           | 1.571         | -9                        | 166          | 254.0          | 1.300         | 5                         |
| 117          | 76.0           | 1.541         | -6                        | 167          | 253.6          | 1.270         | 1                         |
| 118          | 75.8           | 1.511         | -7                        | 168          | 253.2          | 1.241         | -9                        |
| 119          | 75.5           | 1.482         | -4                        | 169          | 252.8          | 1.211         | -3                        |
| 120          | 75.1           | 1.452         | -3                        | 170          | 252.3          | 1.182         | -4                        |



Table 2. Continued.

| No. | Position angle | $R/R_{\odot}$ | $v$<br>km s <sup>-1</sup> | No. | Position angle | $R/R_{\odot}$ | $v$<br>km s <sup>-1</sup> |
|-----|----------------|---------------|---------------------------|-----|----------------|---------------|---------------------------|
| (1) | (2)            | (3)           | (4)                       | (1) | (2)            | (3)           | (4)                       |
| 171 | 104.1          | 1.567         | 7                         | 221 | 214.4          | 1.353         | 6                         |
| 172 | 104.4          | 1.537         | 1                         | 222 | 213.3          | 1.335         | 4                         |
| 173 | 104.7          | 1.507         | 5                         | 223 | 212.2          | 1.319         | -3                        |
| 174 | 105.0          | 1.478         | -4                        | 224 | 211.0          | 1.303         | -6                        |
| 175 | 105.3          | 1.448         | 1                         | 225 | 207.4          | 1.259         | -1                        |
| 176 | 105.6          | 1.418         | 14                        | 226 | 204.8          | 1.232         | -1                        |
| 177 | 106.0          | 1.388         | -7                        | 227 | 202.2          | 1.208         | 12                        |
| 178 | 106.3          | 1.359         | -2                        | 228 | 198.0          | 1.177         | 1                         |
| 179 | 106.6          | 1.329         | -8                        | 229 | 195.1          | 1.160         | -2                        |
| 180 | 107.0          | 1.300         | -3                        | 230 | 190.6          | 1.140         | 1                         |
| 181 | 107.4          | 1.270         | -2                        | 231 | 182.9          | 1.124         | 4                         |
| 182 | 107.8          | 1.241         | -17                       | 232 | 175.0          | 1.128         | -1                        |
| 183 | 108.2          | 1.211         | -11                       | 233 | 167.4          | 1.153         | -7                        |
| 184 | 108.7          | 1.182         | -6                        | 234 | 165.9          | 1.160         | -13                       |
| 185 | 109.2          | 1.153         | -3                        | 235 | 164.5          | 1.168         | -1                        |
| 186 | 109.7          | 1.124         | -10                       | 236 | 163.0          | 1.177         | -3                        |
| 187 | 110.2          | 1.095         | -8                        | 237 | 161.6          | 1.187         | -8                        |
|     | Slit II (2)    |               |                           | 238 | 160.2          | 1.197         | -8                        |
|     |                |               |                           | 239 | 158.8          | 1.208         | -1                        |
|     |                |               |                           | 240 | 157.5          | 1.220         | 4                         |
| 188 | 247.1          | 1.626         | -3                        | 241 | 156.2          | 1.232         | 6                         |
| 189 | 246.6          | 1.598         | -5                        | 242 | 154.9          | 1.245         | 8                         |
| 190 | 246.2          | 1.570         | -4                        | 243 | 153.6          | 1.259         | 11                        |
| 191 | 245.7          | 1.542         | 0                         | 244 | 152.4          | 1.273         | 14                        |
| 192 | 245.2          | 1.514         | 0                         | 245 | 151.2          | 1.288         | 7                         |
| 193 | 244.7          | 1.486         | 4                         |     |                |               |                           |
| 194 | 244.2          | 1.459         | 7                         | 246 | 150.0          | 1.303         | 7                         |
| 195 | 242.5          | 1.376         | 8                         | 247 | 148.8          | 1.319         | 13                        |
| 196 | 241.9          | 1.349         | 3                         | 248 | 147.7          | 1.335         | 10                        |
| 197 | 241.3          | 1.322         | 4                         | 249 | 146.6          | 1.353         | 5                         |
| 198 | 240.6          | 1.296         | 1                         | 250 | 145.6          | 1.370         | 3                         |
| 199 | 239.9          | 1.269         | 4                         | 251 | 144.5          | 1.387         | 14                        |
| 200 | 239.2          | 1.242         | 5                         | 252 | 143.5          | 1.406         | 5                         |
| 201 | 238.4          | 1.216         | 0                         | 253 | 142.5          | 1.425         | -1                        |
| 202 | 237.6          | 1.190         | 5                         |     |                |               |                           |
| 203 | 117.3          | 1.431         | 1                         |     | Slit I (2)     |               |                           |
| 204 | 117.9          | 1.404         | 3                         | 254 | 208.8          | 1.590         | 3                         |
| 205 | 118.5          | 1.376         | 2                         | 255 | 207.8          | 1.576         | 1                         |
| 206 | 119.1          | 1.349         | -1                        | 256 | 206.8          | 1.562         | 8                         |
| 207 | 119.7          | 1.322         | 1                         | 257 | 205.8          | 1.548         | 3                         |
| 208 | 120.4          | 1.296         | 0                         | 258 | 204.8          | 1.536         | 3                         |
| 209 | 121.1          | 1.269         | 1                         | 259 | 203.7          | 1.523         | 6                         |
| 210 | 121.8          | 1.243         | -4                        | 260 | 202.6          | 1.511         | 3                         |
| 211 | 122.6          | 1.217         | -1                        | 261 | 201.5          | 1.500         | 4                         |
| 212 | 123.4          | 1.190         | -8                        | 262 | 200.4          | 1.489         | 6                         |
| 213 | 124.2          | 1.165         | -8                        | 263 | 199.3          | 1.479         | 4                         |
| 214 | 125.0          | 1.139         | -8                        | 264 | 198.2          | 1.469         | 6                         |
| 215 | 126.0          | 1.114         | -4                        | 265 | 197.0          | 1.460         | 10                        |
| 216 | 126.9          | 1.089         | 1                         | 266 | 195.9          | 1.452         | 11                        |
|     | Slit I (1)     |               |                           | 267 | 194.7          | 1.444         | 8                         |
|     |                |               |                           | 268 | 193.5          | 1.437         | 5                         |
|     |                |               |                           | 269 | 192.3          | 1.430         | -1                        |
| 217 | 218.5          | 1.425         | 7                         | 270 | 191.1          | 1.424         | 9                         |
| 218 | 217.5          | 1.406         | 8                         |     |                |               |                           |
| 219 | 216.5          | 1.387         | 12                        | 271 | 189.9          | 1.419         | 4                         |
| 220 | 215.5          | 1.370         | 8                         | 272 | 188.6          | 1.414         | -7                        |

Table 2. Concluded.

| No. | Position angle | $R/R_{\odot}$ | $v$<br>km s <sup>-1</sup> | No. | Position angle | $R/R_{\odot}$ | $v$<br>km s <sup>-1</sup> |
|-----|----------------|---------------|---------------------------|-----|----------------|---------------|---------------------------|
| (1) | (2)            | (3)           | (4)                       | (1) | (2)            | (3)           | (4)                       |
| 273 | 187.4          | 1.410         | -5                        | 287 | 167.5          | 1.437         | -4                        |
| 274 | 186.1          | 1.407         | -3                        | 288 | 166.3          | 1.444         | -1                        |
| 275 | 184.9          | 1.404         | -3                        | 289 | 165.1          | 1.452         | 2                         |
|     |                |               |                           | 290 | 164.0          | 1.460         | -3                        |
| 276 | 183.6          | 1.402         | 1                         |     |                |               |                           |
| 277 | 182.4          | 1.401         | 0                         | 291 | 162.8          | 1.469         | -2                        |
| 278 | 181.1          | 1.400         | 2                         | 292 | 161.7          | 1.479         | -1                        |
| 279 | 179.9          | 1.400         | 2                         | 293 | 160.6          | 1.489         | -2                        |
| 280 | 178.6          | 1.401         | 5                         | 294 | 159.5          | 1.500         | -1                        |
|     |                |               |                           | 295 | 158.4          | 1.511         | -6                        |
| 281 | 174.9          | 1.407         | 7                         |     |                |               |                           |
| 282 | 173.6          | 1.410         | 6                         | 296 | 157.3          | 1.523         | -5                        |
| 283 | 172.4          | 1.414         | 4                         | 297 | 156.3          | 1.535         | -9                        |
| 284 | 171.1          | 1.419         | 3                         | 298 | 155.2          | 1.548         | -5                        |
| 285 | 169.9          | 1.424         | 5                         | 299 | 154.2          | 1.562         | -5                        |
|     |                |               |                           | 300 | 153.2          | 1.576         | -5                        |
| 286 | 168.7          | 1.430         | 2                         |     |                |               |                           |

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### References

- Chandrasekhar, T., Desai, J. N., Angreji, P. D. 1981, *Appl. Opt.*, **20**, 2172.  
 Delone, A. B., Makarova, E. A. 1969, *Solar Phys.*, **9**, 116.  
 Jarrett, A. H., von Klüber, H. 1955, *Mon. Not. R. astr. Soc.*, **115**, 343.  
 Jarrett, A. H., von Klüber, H. 1961, *Mon. Not. R. astr. Soc.*, **122**, 223.  
 Jordan, C. 1969, *Mon. Not. R. astr. Soc.*, **142**, 501.  
 Liebenberg, D. H., Bessey, R. J. Watson, B. 1975, *Solar Phys.*, **44**, 345.  
 Livingston, W., Harvey, J., Doe, L. 1970, *Solar Eclipse 1970 Bulletin F*, National Science Foundation, Washington, p. 72.  
 Marshall, P. M., Henderson, G. 1973, *Solar Phys.*, **33**, 153.